

Sliding Mode Control Based on RBF Neural Network for Parallel Machine Tool

Jiye Yang¹, Yongfeng Cui^{2,*} and Miaochao Chen³

¹School of Basic Education, Jiangsu Food & Pharmaceutical Science College, Huaian, 223000, P. R. China; ²School of Computer Science and Technology, Zhoukou Normal University, Henan, 466001, P. R. China; ³Department of Mathematics, Chaohu University, Hefei, 238000, P. R. China

Abstract: The hydraulic control system, an important composition of parallel machine tool, is a high order, nonlinear, parameter uncertain system, which seriously affects the dynamic performance of a machine tool, so it is very difficult to gain good performance with traditional control methods. The sliding mode control method based on RBF neural network is proposed in this paper. From the simulation results we can obtain that the proposed method is better than the traditional sliding model control method. Moreover, the result validates the proposed method of Hydraulic system for parallel machine tool and also provides the theoretical and experimental basis.

Keywords: Hydraulic servo system, parallel machine tool, RBF neural network, SMC

1. INTRODUCTION

Research about the parallel mechanism can be traced back to the 19th century. Gough produced a tire test device by using the parallel mechanism in 1949. The British engineer, Stewart, has published a paper entitled “a platform with six degrees of freedom” [1]. The above mentioned Stewart platform consisted of the upper and lower platforms and six struts. These six struts are cylinders with pistons inside to afford them independent movement. The struts are coupled by the upper and lower platform and ball joints and Hooke hinge. The lower platform is fixed and the upper platform can move at six degrees of freedom. [2].

Parallel Machine Tool, which is based on the principle of the parallel mechanism in Stewart’s platform (Fig. 1), is derived from the combination of parallel robot mechanism and machine tools. It has high stiffness, high bearing capacity, high accuracy of positioning and smaller work space, compared with the traditional serial mechanism, and it can reduce the static error and dynamic error of machine tools and robots [3]. The flow-pressure and oil leakage of the servo system causes it to have many uncertainties and highly nonlinear characteristics. Therefore, it is difficult for the traditional design methods of control system to meet the control requirements of the parallel robot with six degrees of freedom [4].

In recent years, experts conducted a theoretical analysis and experiments to research parallel robots with six degrees of freedom on robust optimal control [5], two degrees of freedom PID control, adaptive control before the disturbance

force feed forward compensation control and so forth [6]. They obtained some guidance results, but the control effect is still difficult to meet the actual requirements.

Sliding mode control [7-9] is robust with respect to system uncertainties by the use of switching control. But it has disadvantage of chattering [10, 11]. In order to reduce the chattering of the servo system, a sliding mode control algorithm with RBF neural network [12, 13] is proposed in this paper, and the chattering can be reduced effectively.

2. SYSTEM COMPONENTS

The parallel robot’s control system can be divided into five parts: the control computer functions, electro-hydraulic servo control unit, actuator unit, hydraulic system

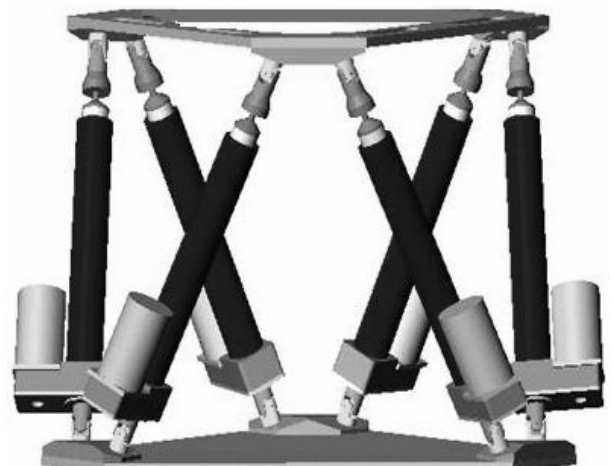


Fig. (1). Stewart platform.

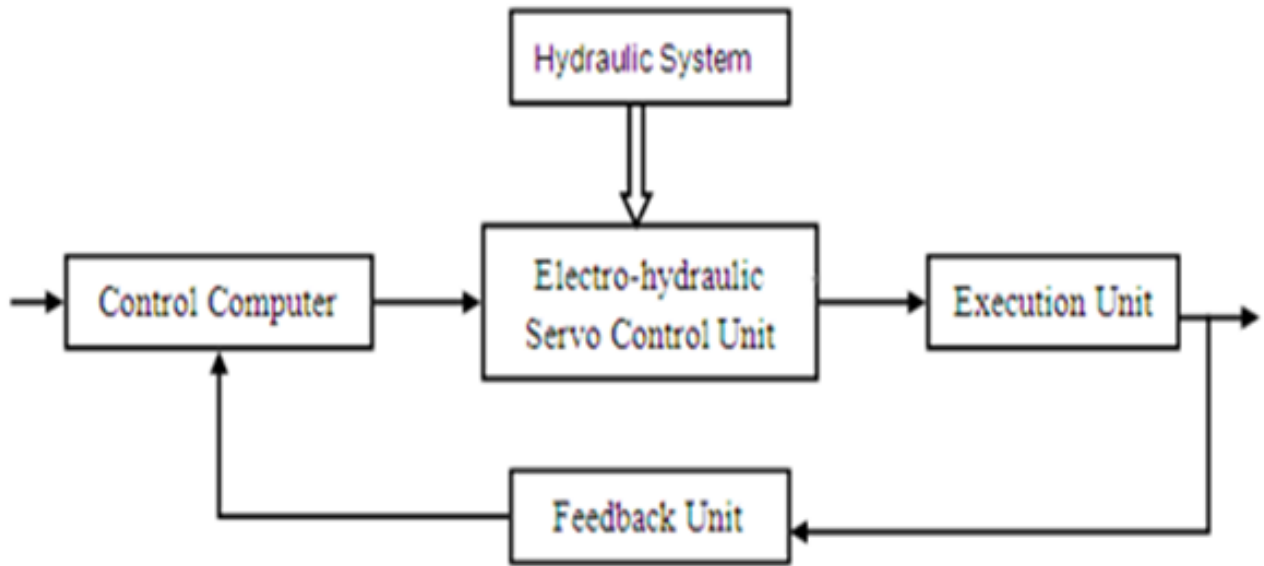


Fig. (2). The figure of components.

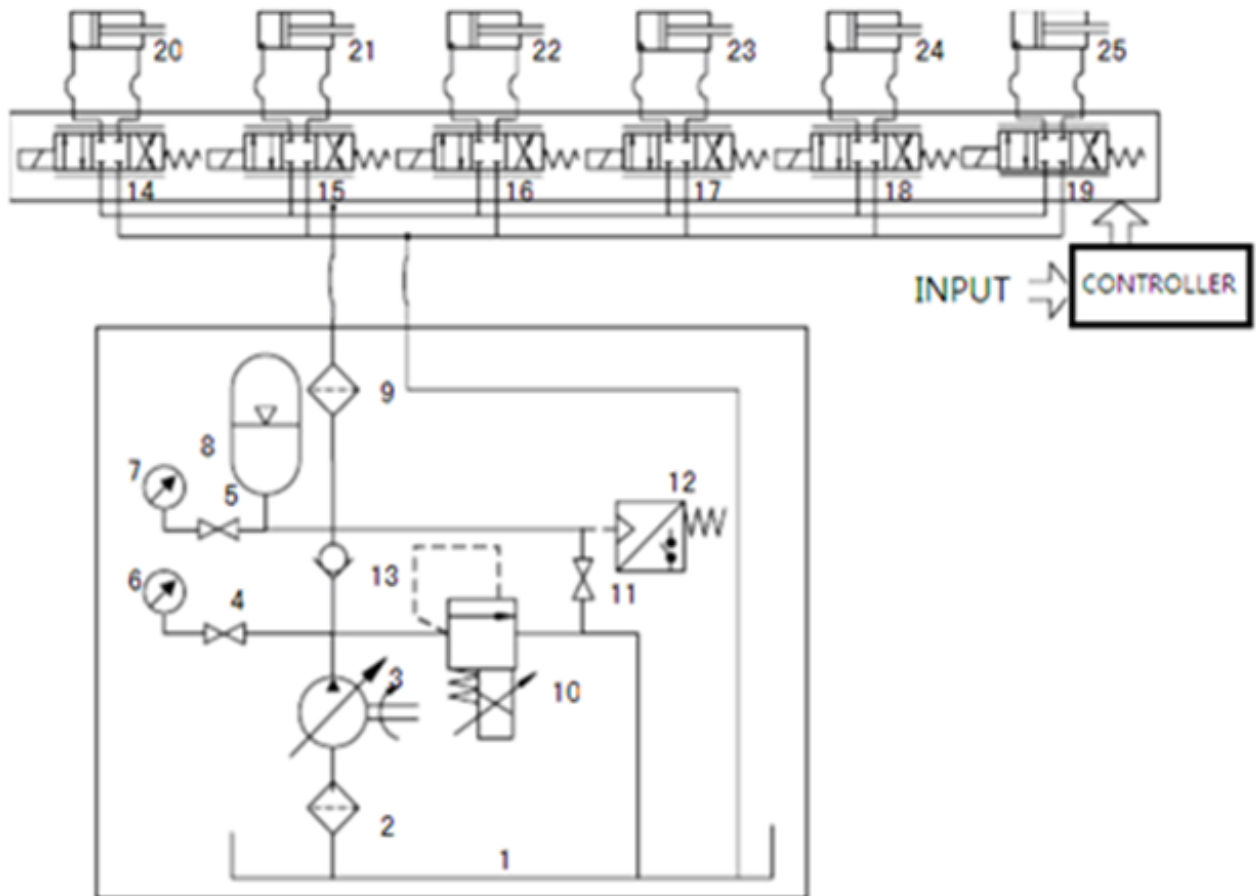


Fig. (3). Hydraulic system of the parallel robot with 6-DOF.

and the feedback unit. The schematic of components are shown in Fig. (2).

The parallel robot with 6-DOF is driven by using hydraulic force, the six hydraulic cylinders control the movement of the

platform, the movable platform (translational and rotational) can move in the six degrees of freedom, the entire hydraulic system consists of hydraulic stations, servo valve, hydraulic cylinder hydraulic servo controllers and components (Fig. 3) [14].

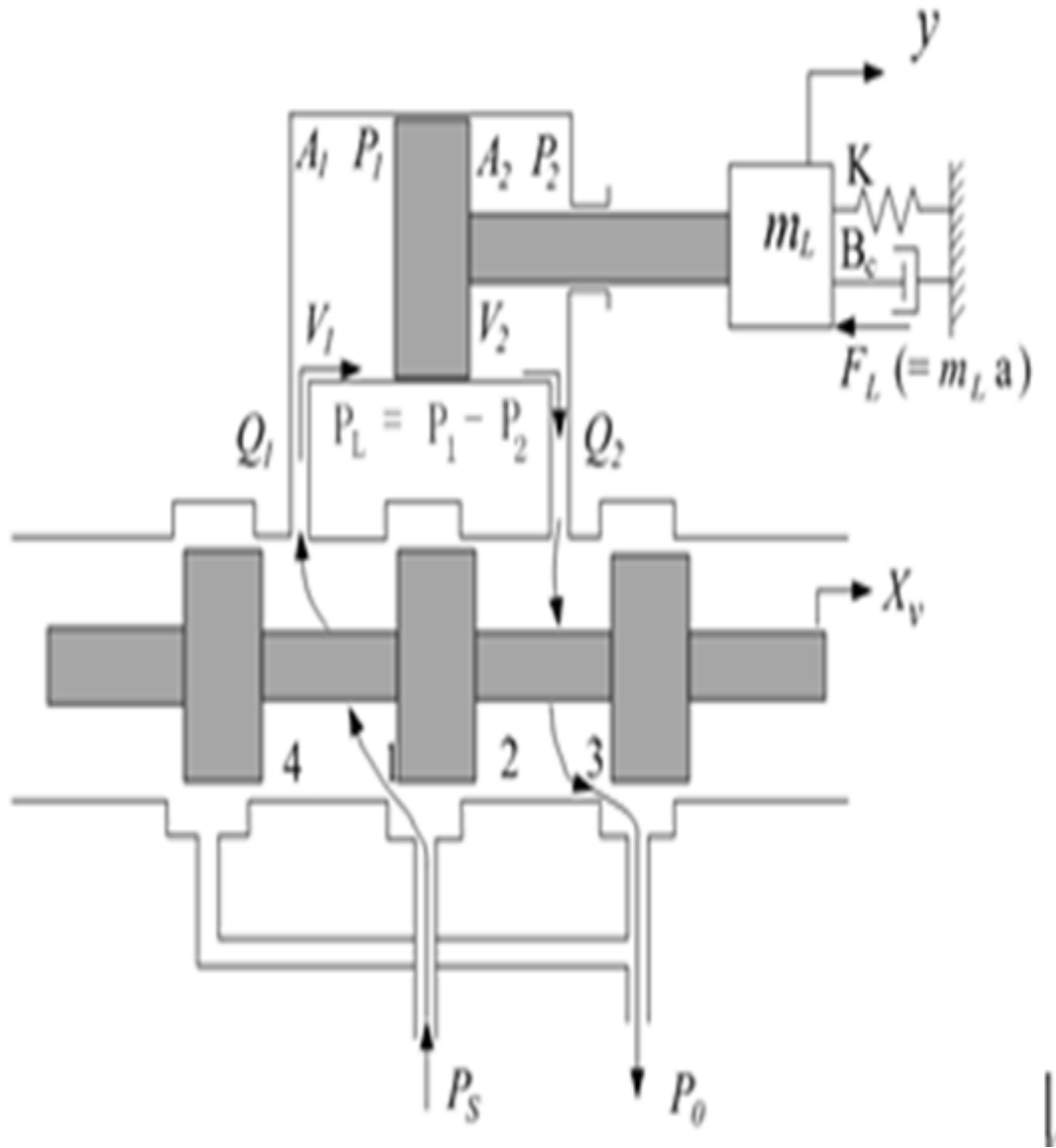


Fig. (4). Schematic diagram for valve controlled asymmetrical cylinder.

3. MATHEMATICAL MODEL

The Hydraulic cylinder servo system of Stewart platform consists of servo valve, hydraulic cylinder, load and so forth, The structure of the valve controlled asymmetrical cylinder is shown in Fig. (4).

Assumption: Four orifice port of the servo valve are matched and symmetrical. The supply pressure P_S is constant and the return oil pressure P_0 is zero.

Based on the above assumptions, the dynamic equation for the valve-controlled valve controlled asymmetrical cylinder can be obtained.

The flow equation of the hydraulic cylinder is given as:

$$= K_q x_v - K_c p_L \tag{1}$$

2) Continuity equation is given as:

$$Q_I = A_1 \frac{dy}{dt} + \frac{V_1}{2(1+n^2)\beta_e} \frac{dp_L}{dt} + C_{ic} p_L + C_{ic1} p_s \tag{2}$$

3) The force balance equation of hydraulic cylinder is given as:

$$= m_L \frac{d^2 y}{dt^2} + B_c \frac{dy}{dt} + Ky + F_L \tag{3}$$

With Laplace transformation for (1), (2), (3),

$$\begin{cases} Q_I = K_e X_v - K_c p_L \\ Q_I = A_I s Y + \frac{V_f}{2(1+n^2)\beta_e} s p_L + C_{fc} p_L + C_{fc} p_s \\ A_I p_L = (m_I s^2 + B_c s + K) Y + F_I \end{cases} \tag{4}$$

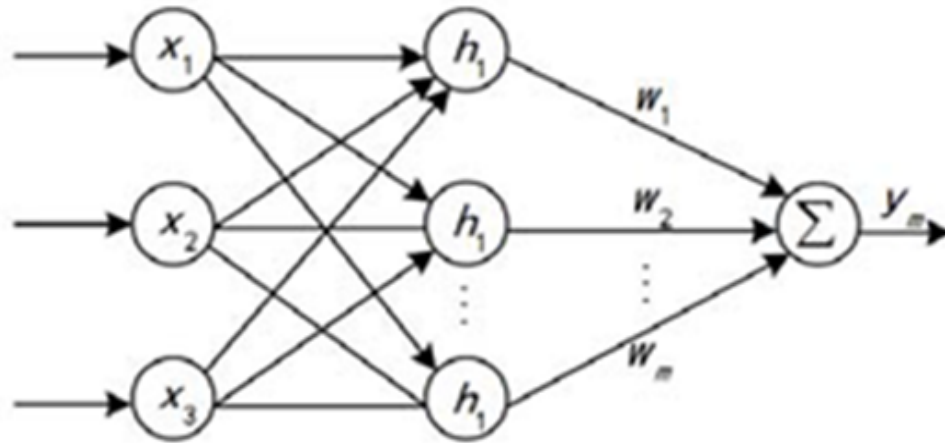


Fig. (5). The scheme diagram of RBF Neural Network.

$$\frac{Y}{X_v} = \frac{\frac{K_q}{A_1}}{s(\frac{s^2}{\omega_k^2} + \frac{2\xi_k}{\omega_k} s + 1)} \tag{5}$$

Where

$$\omega_k = \sqrt{\frac{2(1+n^2)\beta_e A_1^2}{m_I V_t}}$$

$$+ \frac{K_c + C_{tc}}{A_1} \sqrt{\frac{(1+n^2)\beta_e m_{II}}{2V_t}}$$

The transfer function of the valve-controlled valve controlled asymmetrical cylinder can be obtained [3].

4. NEURAL NETWORK SLIDING MODE CONTROL BASED ON RBF

The Radial Basis Function (RBF) is a three layered feed forward network with a single hidden layer (Fig. 5), and it is a kind of local approximation of the neural network. For the practical application, the object features and models are changed frequently but changing slowly. Setting and well optimized SMC parameters may no longer have a very good control effect after a period of time [10, 14-16]. The neural network intelligence SMC controller can identify the model and features of the controlled object through identifier [17]. There are many functional forms of RBF neural network, Gauss function was selected in this article as the hidden layer node function according to its unique advantages. The network input is given as

$$X = [x_1 \quad x_2 \quad \dots \quad x_n]^T,$$

the hidden layer of network output is given as

$$H = [h_1 \quad h_2 \quad \dots \quad h_m]^T,$$

the gauss function is given as \$h_j\$.

$$h_j = \exp\left(-\frac{\|X - C_j\|^2}{2b_j^2}\right) \quad (j = 1, 2, \dots, m) \tag{6}$$

Where $C_j = [c_{j1} \quad c_{j2} \quad \dots \quad c_{jn}]^T$,

$$b_j = [b_{j1} \quad b_{j2} \quad \dots \quad b_{jn}]^T,$$

and the number of hidden layer is given as m.

$$W = [w_1 w_2 \dots w_m]^T \tag{7}$$

The network output is given as:

$$u_n(k) = w_1 h_1 + w_2 h_2 + \dots + w_m h_m \tag{8}$$

The RBF network output is given as:

$$x_n(1) = s(k), x_n(2) = s(k) - s(k-1) \tag{9}$$

Aimed at the output of the RBF network, the sliding mode controller is designed as following, namely

$$u = \sum_{j=1}^m w_j \exp\left(-\frac{\|s - c_j\|^2}{b_j}\right) \tag{10}$$

The BRF network's weights adjustment index is given as:

$$E = s(t)\dot{s}(t) \tag{11}$$

Namely

$$= -\eta \frac{\partial s(t)\dot{s}(t)}{\partial u(t)} \frac{\partial u(t)}{\partial w_j(t)} \quad (\eta > 0) \tag{12}$$

Because of

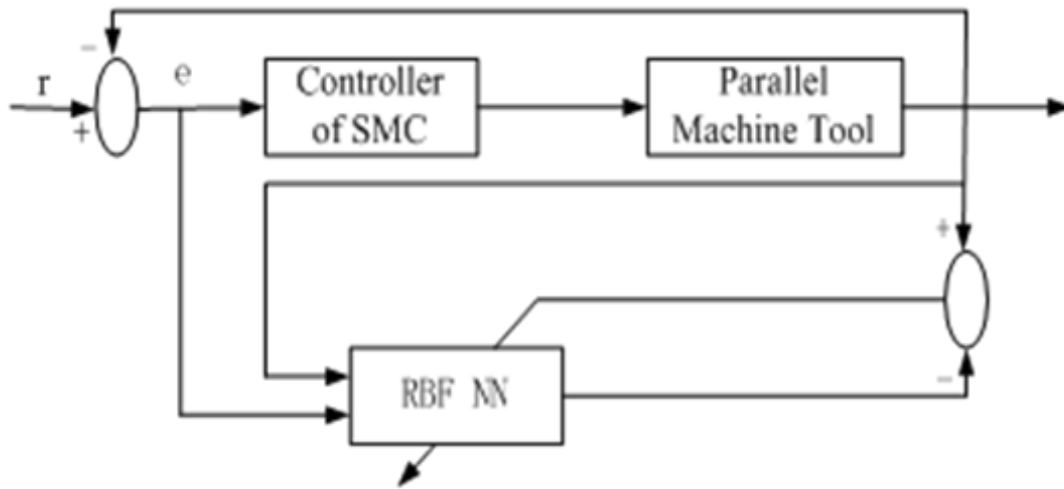


Fig. (6). The structure of sliding mode controller with RBF neural sliding mode controller.

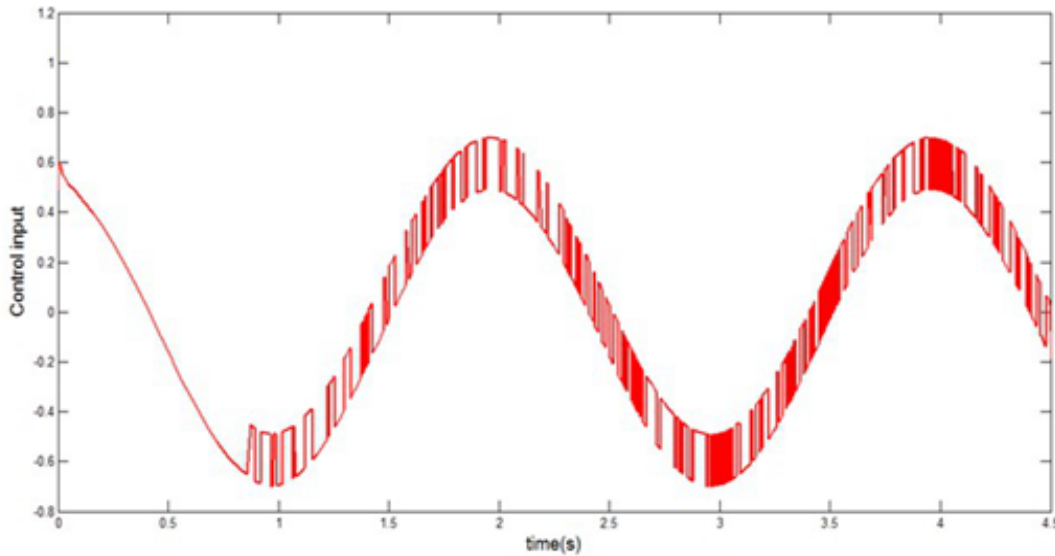


Fig. (7). Control input with SMC.

$$\frac{\partial s(t)\dot{s}(t)}{\partial u} = s(t) \frac{\dot{s}(t)}{\partial u} = -bs(t) \tag{13}$$

$$\frac{\partial u(t)}{\partial w_j(t)} = \exp\left(-\frac{\|s - c_j\|^2}{b_j}\right) \tag{14}$$

The learning algorithm of network weights is given as:

$$dw_j = \gamma s(t) \exp\left(-\frac{\|s - c_j\|^2}{b_j}\right) = \gamma s(t) h_j(s) \tag{15}$$

The structure of sliding mode controller with RBF neural sliding mode controller is shown in Fig. (6),

5. NUMERICAL SIMULATION

In this paper the MATLAB is used to make simulation for the hydraulic servo system to confirm the effectiveness of the controller. Through looking up the corresponding parameters of hydraulic servo system for the parallel machine tool, the transfer function of system is given as following.

$$G(s) = \frac{13341}{s(s^2 + 56.2s + 6542)} \tag{16}$$

Based on the RBF neural sliding mode control, the input of RBF network is given as $[x_1, x_2, x_3]$.

The initial value of weights w is $[0.1, 0.1, 0.1]^T$, disturbance and uncertain item are selected as $0.5\sin(2\pi t)$,

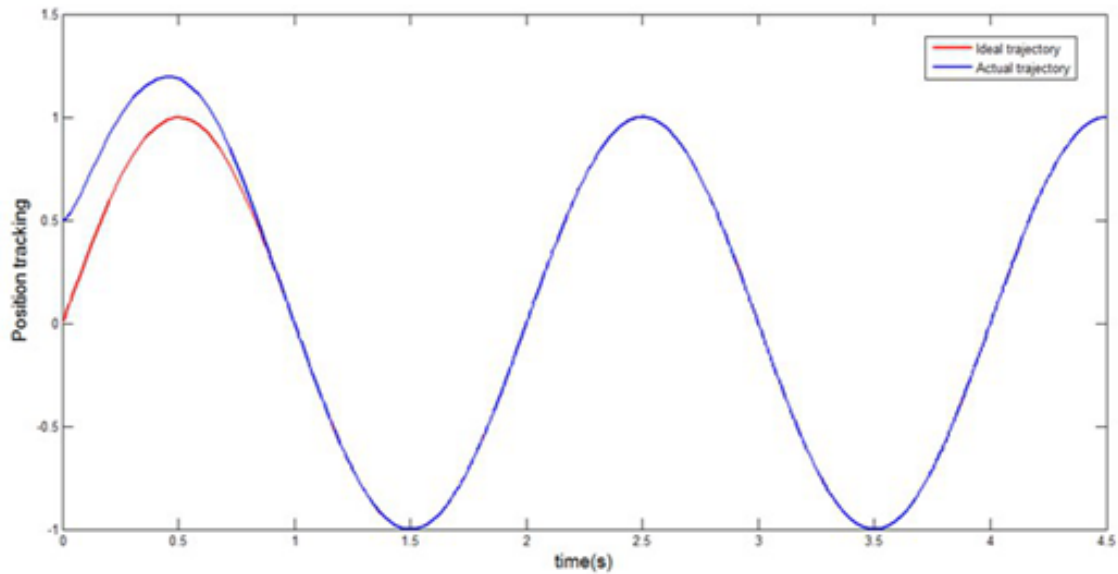


Fig. (8). Position tracking with SMC.

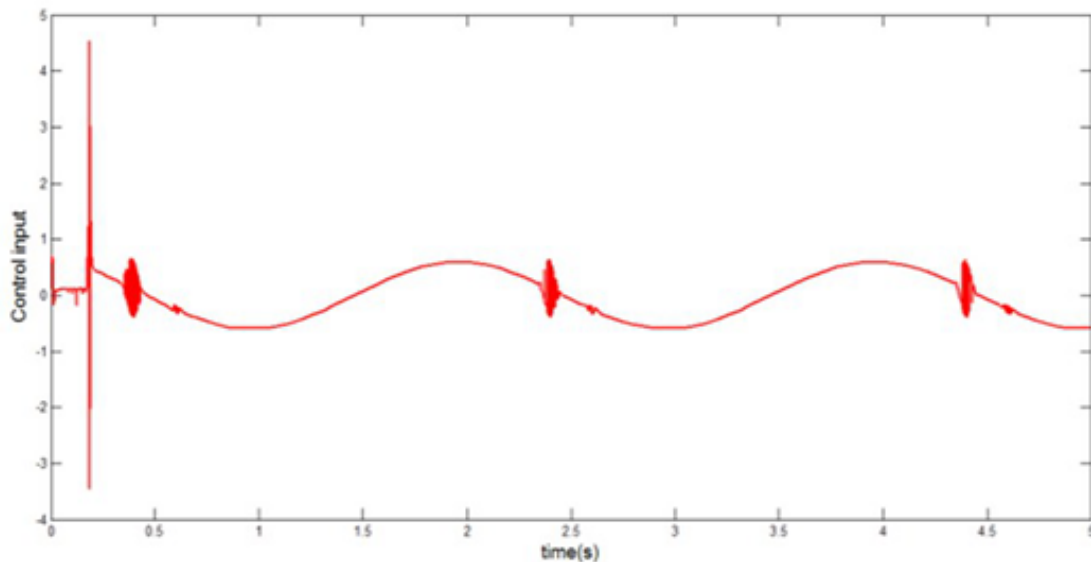


Fig. (9). Control input with SMC Based RBF.

$k_1 = 100, k_2 = 200, c = 30$ the position index is $\sin(\pi t)$. The control input and position tracking of system with SMC is given in Fig. (7 and 8). The control input and position tracking of system with SMC based on RBF neural network is given in Fig. (9 and 10).

6. CURRENT & FUTURE DEVELOPMENTS

Sliding mode control is made robust with respect to system uncertainties through the use of switching control, but it has disadvantage of chattering. In order to reduce the chattering of servo system, the sliding mode control method based on RBF neural network is proposed in this paper. By

analyzing the previous control strategy, we propose the sliding mode control strategy based on RBF neural network, which makes SMC optimized by the RBF neural network. From the simulation results we obtained the performance of the proposed controller has some effectiveness. Moreover, the proposed method validates the Hydraulic system of parallel machine tool and also provides its theoretical and experimental basis.

According to the current development condition, the main developmental directions of the sliding mode control system are stated below.

1. Adjusting the term gain switching Online is an effective method to eliminate chattering. We can realize the

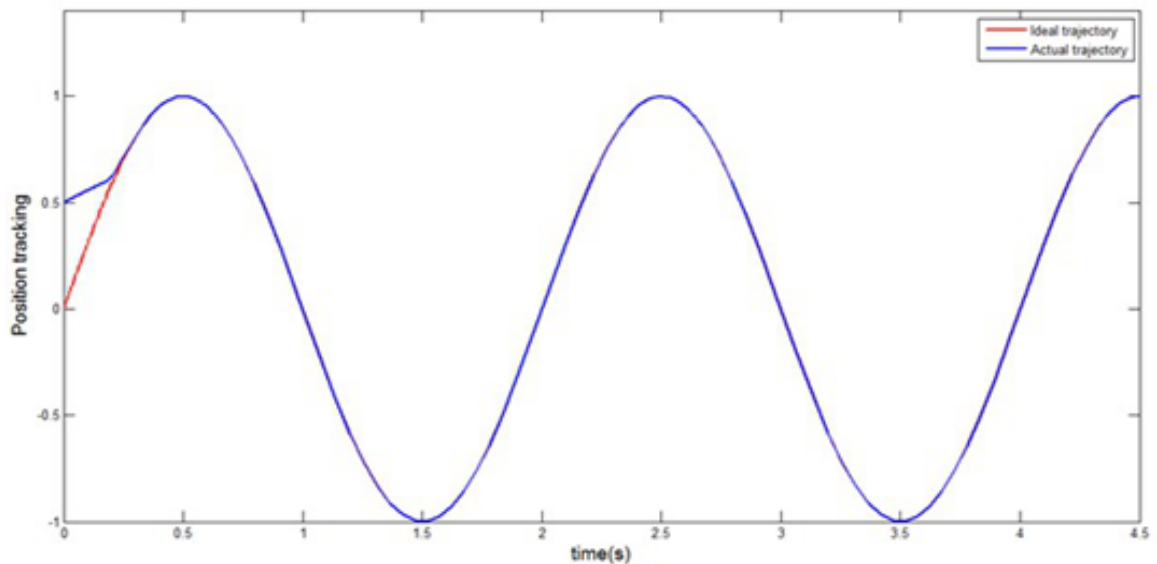


Fig. (10). Position tracking with SMC Based RBF.

switch gain of online optimization, thus minimizing the term gain switching by use of advanced intelligent methods (fuzzy algorithm [18, 19], neural network and genetic algorithm [20, 21], etc.) of sliding mode control.

2. The theory of terminal sliding mode control needs further development. The terminal sliding mode control method mainly refers to convergence to zero in finite time, how to implement the system state convergence to zero within the limited space is the direction of further development of this method.

3. At present, the new sliding mode control method (such as a Terminal sliding mode control, the inversion of sliding mode control and dynamic sliding mode control, etc.) are mostly in the stage of theoretical research.

4. The new sliding mode control method which is applied to actual engineering system in solving practical engineering problems is the focus of future research. Sliding mode control of high order system which has been proposed recently is one of the promising method; there are many problems that need to be researched. If it can be combined with some new method of sliding mode control in the future, we will be able to get better performance of the new type of sliding mode controller.

CONFLICT OF INTEREST

The authors confirm that this article content has no conflict of interest.

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