

Revisited Kinetic Chain Length and Reactivity Ratio Approaches for Linear Polymers and Copolymers

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Abstract: Two revisited mathematical kinetic relationships were derived, evaluated and applied on linear polymers such as polystyrene and copolymers such as (NIPAAm-*alt*-HEMA) and (MAAm-*alt*-HEMA) copolymers respectively. The validity of these equations was successfully verified. The first relationship, equation 12, interrelates exponentially kinetic chain length, average molecular weight and degree of polymerization of linear polymers with different temperatures. Furthermore; equation 12 could novelly define the rate of polymerization (R_p) and consequently the overall activation energy (ΔE) of the polymerization process could be determined. The second derived relationship interrelates the reactivity ratio product ($r_1 r_2$) of two monomers interacting with each other, with different temperature. Application of equation 16 could determine the behavioral sequence of monomer 1 toward monomer 2 in the copolymerization process. The value of $(E_{12}+E_{21})-(E_{11}+E_{22})$ could result with the determination of type of copolymers formed. The reactivity ratio values for (NIPAAm-*alt*-HEMA) and (MAAm-*alt*-HEMA) copolymers were determined using Kelen-Tudos technique.

Keywords; Kinetic chain length, reactivity ratio, Theoretical Kinetic approach.

INTRODUCTION

Radical kinetic chain polymerization, as one of the most crucial techniques in the control and optimization of recent polymeric industries, is always finding renewable generated ideas and interest in the theory and kinetic parameters of polymerization processes. This major concern is due to the outstanding applications, practical use, and relatively easy control [1] of radical reactions. This concern have further oriented us to derive practical, adequate and easily handled kinetic relationships for practical purposes. The determination of polymerization rate in equation 1 at different temperatures, in *Arrhenius equation*, implies the determination of k_p , k_d , and k_t respectively.

$$\ln \left(k_p \left(\frac{k_d}{k_t} \right)^{1/2} \right) = \ln \left(A_p \left(\frac{A_d}{A_t} \right)^{1/2} \right) - \frac{\left(E_p + \frac{E_d}{2} - \frac{E_t}{2} \right)}{RT} \quad (1)$$

where k_p , k_d , and k_t are rate constants for propagation, initiator dissociation and termination respectively. Since rate of polymerization (R_p) is given by

$$R_p = k_p \left(\frac{fk_d[I]}{k_t} \right)^{1/2} \quad (2)$$

Substituting eq'n (2) in (1) yields;

$$\ln R_p = \ln \left(A_p \left(\frac{A_d}{A_t} \right)^{1/2} \right) + \ln (f[I]^{1/2}[M]) - \frac{\Delta E_p}{RT} \quad (3)$$

The exact determination of polymerization rate (R_p) is the most important factor in *Arrhenius equation*, due to consequence determination of exact overall activation energy. In

the literature R_p were determined using spectroscopic means such as UV-Vis [2], FTIR [3], NMR [4], XRD [5], mass spectrometry [6] and TGA [9], or by Laser beam technology [8-9], or using conventional %Conversion versus Time plot by precipitation of polymers [10], where R_p is determined from the non-steady state curve.

Consequently the determination the overall activation energy $\Delta E_a = E_p + (E_d/2) - (E_t/2)$ describes the kinetic changes in the polymerization process whether it shows an *Arrhenius* behavior (i.e. $\Delta E_a > 0$), which implies that the reaction rate increase as a result of increasing temperature, or *non-Arrhenius* behavior (i.e. $\Delta E_a < 0$), which subsequently implies that reaction rate decreases as a result of increasing temperature. The overall activation energy is associated with E_p , E_d , and E_t values, which dramatically change with many factors such as monomer structure and geometry, initiator type, temperature, polymerization time, and chain transfer agent.

The aim of this work is to derive, investigate and apply revisited kinetic relationships through raising a new definition of rate of polymerization (R_p) for linear polymerization and copolymerization processes, applying that into *Arrhenius* pattern and eventually investigating the consistency and genuinity of such relationships.

EXPERIMENTAL

Materials

Styrene (99%, Acros), *Methacrylamide* (MAAm) (99%, Fluka), *N*-isopropylacrylamide (NIPAAm) (99%, Acros) and 2-Hydroxyethylmethacrylate (HEMA) (99%, Acros) monomers were kept in refrigerator and used as received, *N,N,N',N'*-Tetraethylenediamine (TEMED) (Sigma-Aldrich) used as an accelerator, was used as received, Potassium peroxodisulfate (KPS) (BDH chemicals Ltd), and benzoylperoxide as an initiator, was further purified by recrystallization. All solvents and other chemicals were of analytical grade.

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Synthesis of Polystyrene (PS)

Styrene monomer were conventionally polymerized under N₂ atmosphere, in bulk, in the temperature range of 60-80 °C using 0.1% benzoylperoxide, where at each time interval 15, 30, 45, 60, 75 min., excess methanol nonsolvent were used to precipitate polystyrene. Continuous washing with methanol were done to remove monomer traces. Polystyrene were then dried and weighed. The weight average molecular weight was determined using light scattering technique [11]. The degree of polymerization were determined from the ratio of absorbance of aliphatic ν_{C=C} of monomer before polymerization and after polymer precipitation.

Synthesis of (NIPAAm-alt-HEMA) and (MAAm-alt-HEMA) Copolymers

0.66, 1.0, 1.3, 1.5, 3.0, and 9.0 molar ratios of NIPAAm to HEMA (i.e. M_{NIPAAm}/M_{HEMA}) and MAAm to HEMA (i.e. M_{MAAm}/M_{HEMA}) as mentioned previously [12, 13], were synthesized as follow; each monomer concentration were dissolved in 25 ml of de-ionized water. The solutions were sparged with N₂ for 5 minutes or until the monomer is dissolved. To each solution a 5 ml of 10 % (wt/wt) KPS and 5 ml of 10 % (wt/wt) TEMED with respect to total monomers weights were added under N₂ atmosphere. Then the mixture was set in 250 ml round bottom flask and sealed under N₂ atmosphere for 3.5 hours in water-bath fixed at 30 °C. After the copolymerization was complete, the product was poured to an excess of chloroform, stirred for 15 min, and washed with hot de-ionized water to remove homopolymers, then filtered and dried in an oven at 80 °C for 8-12 hours. The samples were further purified *via* centrifugation. The weight average molecular weight was determined using light scattering technique [11]. Reactivity ratios r₁ and r₂ values were determined using Kelen-Tudos technique [14] at 20-40 °C temperature range for (NIPAAm-alt-HEMA) and at 5-20 °C temperature range for (MAAm-alt-HEMA) copolymers.

THEORETICAL APPROACH (1)

Kinetic chain length (L_{i,t}) is defined as the number of monomers added into a growing macroradical of ith length in unit time interval. The molecular weight of this chain in the same time interval, M_{i,t}, can be described as the kinetic chain length, L_{i,t}, times the molar mass of the repeating unit, M_{ru}, as follows;

$$M_{i,t} = L_{i,t} \times M_{ru} \quad (4)$$

At time ∞, if theoretically assumed all monomers can join all different chains, the overall kinetic chain lengths is then called L_∞ and consequently the average molecular weight can also be called M_∞. Thus the fraction of reacted monomers joining the ith length macroradical chain, p_i, can be presented by dividing the kinetic chain length of ith length macroradical chain, at certain time (L_{i,t}), to the overall kinetic chain lengths L_∞. Consequently this fraction can be described by the ratio of molecular weight of ith length macroradical chain at certain time (M_{i,t}) by the molecular weight M_∞. Thus the relation becomes;

$$p_i = \frac{M_{i,t}}{M_{\infty}} = \frac{L_{i,t}}{L_{\infty}} \quad (5)$$

The degree of polymerization (DP_i) is defined as ratio of initial monomer conc., [A]₀, to monomer conc. at polymerization time t, [A]_t, (i.e. DP_i = [A]₀ / [A]_t). The reciprocal of DP_i presents the fraction of unreacted monomers (i.e. the monomers that did not join the ith length macroradical chain, where i present the number of repeating units in the macroradical chain). Hence, the fraction of reacted monomers joining the macroradical chain, p_i, is equal to 1-(1/DP_i). Thus it can be equalized with equation 5 as follows;

$$\frac{M_{i,t}}{M_{\infty}} = 1 - \frac{1}{DP_i}$$

$$M_{i,t} = M_{\infty} \cdot \left(1 - \frac{1}{DP_i}\right) \quad (6)$$

Number average molecular weight (\overline{M}_n) [15] is defined in equation 7, where M_i is the molecular weight of ith length chain, n_i is number of chains with ith length, and N_T is the total number of chains with different chain lengths. Thus the fraction n_i/N_T represents the fraction of chains with ith length with respect to total different length chains.

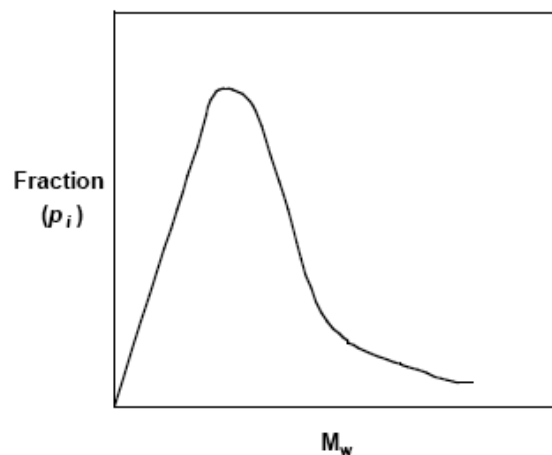
$$\overline{M}_n = \frac{\sum_i M_i n_i}{\sum_i n_i}$$

$$= \frac{M_1 n_1}{N_T} + \frac{M_2 n_2}{N_T} + \frac{M_3 n_3}{N_T} + \dots + \frac{M_n n_n}{N_T} \quad (7)$$

Furthermore; it is known that different chain lengths (i.e. different molecular weight chains) in any polymer follows Boltzmann distribution curve (Scheme 1) and consequently it follows the Boltzmann distribution law [16], where fraction of chains can be presented in an exponential form as follows;

$$\frac{n_i}{N_T} = \frac{e^{-\frac{E_i}{RT}}}{\sum e^{-\frac{E_i}{RT}}}$$

$$= e^{-\frac{\Delta E}{RT}} \quad (8)$$



Scheme 1. Molecular weight distribution curve of polystyrene.

For which E_i presents the activation energy required for monomer to join an i^{th} length macroradical chain. The different size chains may have different activation energies (i.e. E_i , E_j , E_k , ...) depends on the size length and how much entangled, coalescent, or agglomerated the chain is, in other words the activation energy differs slightly for extended chain that can coalescent, agglomerate, and largely entangled, and consequently ΔE is the resultant overall activation energy required for any monomer to join any chain of any chain length no matter what configuration does it have.

Substituting equation 8 in equation 7 turns to be:

$$\overline{M}_n = (M_1 + M_2 + M_3 + \dots + M_n) \cdot e^{-\frac{\Delta E}{RT}} \quad (9)$$

Again substituting equation 6 in equation 9 gives rise;

$$\begin{aligned} \overline{M}_n &= \left(M_\infty \cdot \left(1 - \frac{1}{DP_1}\right) + M_\infty \cdot \left(1 - \frac{1}{DP_2}\right) + M_\infty \cdot \left(1 - \frac{1}{DP_3}\right) + \dots + M_\infty \cdot \left(1 - \frac{1}{DP_n}\right) \right) \cdot e^{-\frac{\Delta E}{RT}} \\ &= \left(\left(1 - \frac{1}{DP_1}\right) + \left(1 - \frac{1}{DP_2}\right) + \left(1 - \frac{1}{DP_3}\right) + \dots + \left(1 - \frac{1}{DP_n}\right) \right) \cdot M_\infty \cdot e^{-\frac{\Delta E}{RT}} \quad (10) \end{aligned}$$

Thus the molecular weight of any linear polymer at any polymerization time can accordingly be determined through the following relationship;

$$\begin{aligned} M_{i,t} &= \left(1 - \frac{1}{DP_i}\right) \cdot M_\infty \cdot e^{-\frac{\Delta E}{RT}} \\ \frac{M_{i,t}}{\left(1 - \frac{1}{DP_i}\right)} &= M_\infty \cdot e^{-\frac{\Delta E}{RT}} \quad (11) \end{aligned}$$

This linear relationship relates the momentarily change of molecular weight and degree of polymerization with the change of temperature. Hence by taking the natural logarithm for both sides;

$$\ln \left[\frac{M_{i,t}}{\left(1 - \frac{1}{DP_i}\right)} \right] = \ln M_\infty - \frac{\Delta E}{RT} \quad (12)$$

This linear relationship can determine the momentarily rate of polymerization (R_p) and consequently the resulting activation energy (ΔE) at different temperatures can be determined for this type of linear polymerization processes. Furthermore the theoretically assumed molecular weight for all monomers joining different chains at infinite time (M_∞) can also be investigated and determined.

The DP_i at time zero of polymerization has a value of 1.0 (i.e. $[A]_0 = [A]_t$), whereas at time ∞ it has a value of infinity (∞) (i.e. $[A]_t \cong \text{zero}$). The determination of DP_i can be performed through monitoring the disappearance of aliphatic C=C for poly addition type, or monitoring the end group structural changes for poly condensation type, at different time interval through different spectroscopic techniques such as $^{13}\text{C-NMR}$, $^1\text{H-NMR}$, FTIR, and UV-Vis, whereas the molecular weight can be determined through conventional gel

permeation chromatography (GPC), Osmometry, light scattering, and Ubbelohde viscometry techniques.

Fig. (1) shows the $\ln [M_i / (1 - (1/DP_i))]$ versus reciprocal temperature of polystyrene polymerized at different time interval in the temperature range of 60–80 °C.

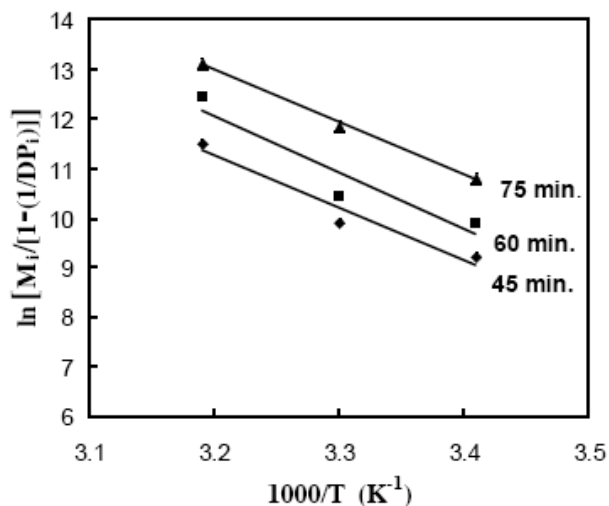


Fig. (1). $\ln [M_i / (1 - (1/DP_i))]$ versus $1/T$ for bulk polymerized polystyrene in different time intervals in the temperature range of 60–80 °C.

It can be clearly seen that the application of equation 12 results with linear determination of the overall activation energies at different time intervals. The overall activation energies determined from Fig. (1) range from 87–95.5 kJ/mol, which is in very good agreement with conventional determination of activation energy of different conformational polystyrenes in the literature [17,18]. Furthermore; the extrapolations of the curves result with almost one intercept value (i.e. M_∞) regardless to the time of polymerization, which again confirms the consistency and rigidity of equation 12 used to show and present the Arrhenius relationship in practical and renewable form.

THEORETICAL APPROACH (2)

It is known the $r_1 = \frac{k_{11}}{k_{12}}$, where k_{11} and k_{12} are the rate

constants of the interaction of a macroradical (M_1^\cdot) with either M_1 or M_2 monomers respectively, and $r_2 = \frac{k_{22}}{k_{21}}$ where k_{22} and k_{21} are the rate constants of the interaction of a macroradical (M_2^\cdot) with either M_2 or M_1 monomers respectively. If Arrhenius equation is applied to the reactivity ratio r_1 and r_2 , then the outcome will be equation 13;

$$r_1 = \frac{k_{11}}{k_{12}} = \frac{A_{11}}{A_{12}} \exp\left(\frac{E_{12} - E_{11}}{RT}\right) \quad (13)$$

Consequently; $r_2 = \frac{k_{22}}{k_{21}}$ becomes;

Table 1. Change of r_1r_2 Product as Temperature Changes for (NIPAAm-*alt*-HEMA) Copolymers

Temperature (°C)	r_1	r_2	r_1r_2
20	0.0034	0.114	0.0003876
30	0.0509	0.427	0.0217343
40	0.0356	0.178	0.0063368

Table 2. Change of r_1r_2 Product as Temperature Changes for (MAAm-*alt*-HEMA) Copolymers

Temperature (°C)	r_1	r_2	r_1r_2
5	0.0334	0.0249	0.0008
10	0.0253	0.0252	0.0006
20	0.0875	0.2042	0.0179

$$r_2 = \frac{k_{22}}{k_{21}} = \frac{A_{22}}{A_{21}} \exp\left(\frac{E_{21} - E_{22}}{RT}\right) \quad (14)$$

Thus r_1r_2 equals;

$$r_1r_2 = \frac{A_{11}A_{22}}{A_{12}A_{21}} \exp\left(\frac{(E_{12} - E_{11}) + (E_{21} - E_{22})}{RT}\right) \quad (15)$$

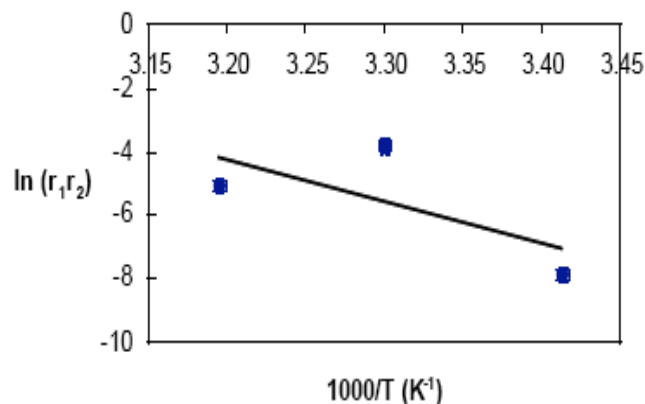
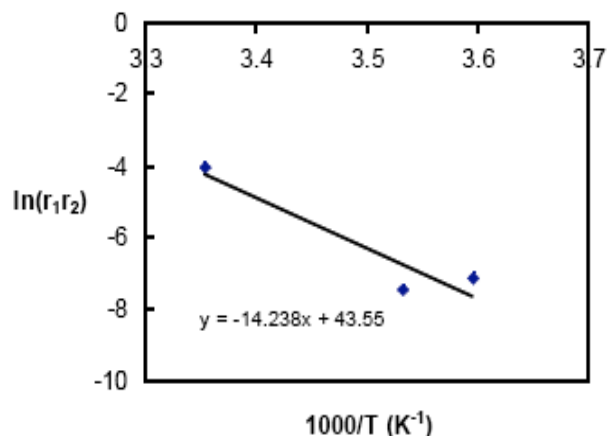
Rearrangement of equation 15 yields;

$$r_1r_2 = \frac{A_{11}A_{22}}{A_{12}A_{21}} \exp\left(\frac{(E_{12} + E_{21}) - (E_{11} + E_{22})}{RT}\right) \quad (16)$$

Equation 16 presents the linear relationship between the natural logarithm of r_1r_2 product ($\ln(r_1r_2)$) with the reciprocal of the temperature in Kelvin ($1/T$), where the activation energy could be determined through the slope value of the curve. The value of the activation energy in eq'n 16 becomes very important because it can show the type of preference of a macroradical (M_1) toward either M_1 or M_2 . If (M_1) macroradical prefers M_2 and (M_2) macroradical prefers M_1 and then the activation energy ($E_{12} + E_{21}$) will be much smaller than ($E_{11} + E_{22}$) and consequently the alternating behavior of copolymer will dominate. Whereas if (M_1) macroradical prefers M_1 and (M_2) macroradical prefers M_2 and then the activation energy ($E_{12} + E_{21}$) will be much larger than ($E_{11} + E_{22}$) and consequently a block or phase separated homopolymer behavior will dominate. Eventually if ($E_{12} + E_{21}$) \approx ($E_{11} + E_{22}$) then the copolymer is said to be random. Table 1 and 2 illustrate change of r_1r_2 product as temperature changes for both copolymers (NIPAAm-*alt*-HEMA) and (MAAm-*alt*-HEMA) [12,13] respectively. The reactivity ratios were determined using Kelen-Tudos technique [14].

Figs. (2 and 3) show the linear relationship of $\ln(r_1r_2)$ versus $1/T$, which is derived from equation 16. The activation energy (i.e. ($E_{12} + E_{21}$) - ($E_{11} + E_{22}$)) of (NIPAAm-*alt*-HEMA) and (MAAm-*alt*-HEMA) copolymer were found to be -109 kJ/mol and -118.4 kJ/mol respectively. Such negative activation energies confirm that ($E_{12} + E_{21}$) \ll ($E_{11} + E_{22}$) in both copolymers, and hence confirms the alternating behavior of the monomers toward each other. Furthermore by

comparing the activation energy values deduced from equation 16 with similar structures mentioned in the literature, it was found that they are in accordance with literature values (i.e. $\Delta E = 97 \pm 5$ kJ/mol [19]).

**Fig. (2).** Change of $\ln(r_1r_2)$ versus $1/T$ for (NIPAAm-*alt*-HEMA) copolymer.**Fig. (3).** Change of $\ln(r_1r_2)$ versus $1/T$ for (MAAm-*alt*-HEMA) copolymer.

From Figs. (2 and 3) it can be clearly seen that not only linear determination of activation energies can be determined but also the type of copolymers formed can be deduced and determined.

CONCLUSIONS

The two revisited mathematical kinetic relationships were derived, evaluated and eventually applied to confirm the consistency, genuinity, and linearity of the formed relationships. The first relationship, equation 12,

$$\ln \left[\frac{M_{i,t}}{\left(1 - \frac{1}{DP_i}\right)} \right] = \ln M_{\infty} - \frac{\Delta E}{RT}$$

which relates the change of molecular weight, degree of polymerization momentarily of linear polymers with temperature, where this linear relationship can determine the overall activation energy of the polymerization process. The validity of this linear relationship was verified using different time intervals bulkily polymerized polystyrene as Fig. (1) shows. The second relationship interrelates the reactivity ratio product ($r_1 r_2$) with temperatures, which again showed a linear relationship, equation 16,

$$r_1 r_2 = \frac{A_{11} A_{22}}{A_{12} A_{21}} \exp \left(\frac{(E_{12} + E_{21}) - (E_{11} + E_{22})}{RT} \right)$$

This linear relationship can determine the activation energy value for the copolymerization process (i.e. $(E_{12} + E_{21}) - (E_{11} + E_{22})$), and consequently the type and sequence of monomers in the copolymer can be described. The validity of this equation were successfully verified for (NI-

PAAm-*alt*-HEMA) and (MAAm-*alt*-HEMA) copolymers respectively.

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