

Disclaimer: This article has been published immediately upon acceptance (by the Editors of the journal) as a provisional PDF from the revised version submitted by the authors(s). The final PDF version of this article will be available from the journal URL shortly after approval of the proofs by authors(s) and publisher.

Logging Evaluation Method for Pore Pressure of Shale Gas Reservoirs— Taking Fuling area, Sichuan Basin as an example

Hao Shibo and Jin Wujun

The Open Petroleum Engineering Journal, Volume 8, 2015

ISSN: 1874-8341

DOI: 10.2174/1874834120150625E018

Article Type: Research Article

Received: November 05, 2014

Revised: January 03, 2015

Accepted: June 23, 2015

Provisional PDF Publication Date: June 25, 2015

© Shibo and Wujun; Licensee Bentham Open.

This is an open access article licensed under the terms of the Creative Commons Attribution Non-Commercial License (<http://creativecommons.org/licenses/by-nc/3.0/>) which permits unrestricted, non-commercial use, distribution and reproduction in any medium, provided the work is properly cited.

Logging Evaluation Method for Pore Pressure of Shale Gas Reservoirs—Taking Fuling area, Sichuan Basin as an example

Hao Shibo, Jin Wujun*

(Petroleum Exploration and development Research Institute, SINOPEC, Beijing 100083)

Abstract

Unconventional oil and gas resources, especially shale gas resources have great potential for exploration and development in China. In Shale gas exploration and development process, reservoir pore pressure is a very important parameter, and the pore pressure prediction can improve the appraisal accuracy of project dessert. This paper analyzes several formation pore pressure calculation methods based on logging data, and optimized the “Equivalent depth method”. The preliminary results show that this method can carry out the accurate evaluation on the abnormal high pressure of the shale gas reservoirs of Fuling area with high calculation precision and application potential.

Key words

Pore pressure, Logging evaluation, Equivalent depth method, Normal compaction trend

1. Introduction and background

Evaluation of formation pore pressure by using well-logging data has the characteristics of continuous analysis data, low cost, and reliable precision^[1-4]. However, most of the existing methods are widely used in conventional reservoirs that have source beds, reservoirs and cap rocks. Yet to see examples of using these methods for the shale gas reservoirs that have the characteristics of generating itself, storing itself and enveloping itself. And according to the current development speed of shale gas, to understand the gas production reasons from the aspects of gas pore pressure, is what we need to do.

Shale gas is natural gas extracted from shale, and mainly exists in the dark mud shale or high carbon mud shale. Shale has changeable mineral composition and complex pore structure, therefore it mainly exists in surfaces of kerogen or clay particles in the adsorbed state, and exists in the cracks, pores and other storage space in the free-state, and also a very small amount of shale gas is present in dissolved state in kerogen or asphalt. The study area of this paper lies in the Fuling area of Sichuan basin, and its good potential of organic rich shale mainly developed in the Longmaxi formation of Silurian to the Wufeng formation of Ordovician. The shale thickness is generally 40m-210m, the TOC content is from 1.0% to 5.0%, porosity ranges from 2% to 7.2%, and the buried depth is in the 2000m to 3000m range. The Longmaxi formation of Silurian is a set of black shale with gray green muddy siltstone. And the lithology of the Wufeng formation of Ordovician is gray dark silty mudstone that contain graptolite fossils.

The mudstone and silty mudstone of the Xiaoheba formation and Hanjiadian formation of the Silurian and the limestone and dolomitic limestone of the Carboniferous covering the Longmaxi formation and Wufeng formation in Fuling area form a very good closed environment. Due to the abundant source in the sedimentary period of Wufeng and Longmaxi formation, the subsidence and accumulation of the sediments was relatively rapid to make the deposition of particles irregular and the drainage capacity weak. With the overlying sedimentary loading continued to increase, this part load was undertaken by the pore fluid and formed an under-compaction. At the same time, the organic matter increased in the sediments with the increasing buried depth and generated hydrocarbon under

certain temperature and pressure condition. This part of hydrocarbon then sharply increased the pore fluid volume and formed abnormal high pressure. Therefore, the under-compaction combining with the hydrocarbon expansion is likely to make shale gas reservoir of the Longmaxi formation form the abnormal high pressure characteristics.

2. Principle and Method of pore pressure analysis

In the buried environment of reservoirs, we believe that the overburden pressure at a certain depth point should be borne together by the reservoir pore pressure and the framework supporting stress. This is based on effective stress theorem proposed by Terzaghi, that is:

$$P_0 = P_e + P_p \quad (1)$$

In the Equation (1), P_0 is the overburden pressure, P_e is the vertical effective stress, P_p is the formation pore pressure.

2.1 The principle and calculation method of comprehensive interpretation

After the in-depth study of the principles of comprehensive interpretation, the writer realized that by the integral of the density logging data can obtain the overburden pressure^[5]. Just try to obtain the vertical effective stress, and then pore pressure can be obtained. More calculation methods of vertical effective stress are all backward-reasoned from the acoustic velocity model of experience that proposed by Eberhart Phillips when he was studying the acoustic velocity model. That is:

$$V_p = A_0 + A_1 \phi + A_2 \sqrt{V_{sh}} + A_3 (p_e - e^{-Dp_e}) \quad (2)$$

In the formula, V_p is acoustic velocity, A_0, A_1, A_2, A_3, D are model coefficients, ϕ is porosity, V_{sh} is clay content, P_e is vertical effective stress. Therefore, the sound velocity in the strata which has normal compaction conditions is related to the factors of lithology, buried depth, the degree of compaction^[6].

The factors affecting the acoustic velocity can be well determined by this model, so the porosity, clay content and vertical effective stress in the study area needs to be measured to determine the model coefficients by the optimal method. Then by using the continuous porosity, clay content and the acoustic velocity curve, the overlying formation pressure data can be calculated, and by inserting the data into the formula (1), the continuous formation pore pressure can be obtained. But, in this study, the measured work of vertical effective stress has not been done in Fuling area, which makes this method lacks certain applicability in the local area.

2.2 The principle and calculation method of “the Eaton method”

In 1972, Eaton established the exponential relationship between formation pore pressure and logging parameters (interval transit time, resistivity)^[7]. According to the experience of the Gulf of Mexico and the research on the rock physical experiment data. This relationship does not change with the variation of lithology or depth, its basic expressional form is:

$$P_p = P_0 - (P_0 - P_w)(\Delta t_n / \Delta t)^E \quad (3)$$

In the formula, P_p is formation pore pressure, the P_0, P_w is respectively the overburden pressure, hydrostatic pressure, Δt is interval transit time at arbitrarily measured depth, Δt_n is interval transit time value under normal compaction condition at the same depth, E is the Eaton power index. The formula (3) shows that the calculation accuracy of formation pore pressure is closely related to the Eaton power index E. According to the existed measured values of the formation pore pressure, the Eaton power index E of formation pressure testing depth of each well in the study area can be induced. However, in this study, there is no effective measured pore pressure data in Fuling area which makes this method not applicable in the local area.

2.3 The principle and calculation method of “equivalent depth method”

The researchers found that, after digging into the acoustic logging data, two points of formation that had same acoustic velocity were encountered in the process of acoustic logging test to a set of more

stable mudstone formation. In this way, the physical properties are the same, which means that the effective stress that is borne by these two mudstone skeleton is the same too. But, the larger part of overburden pressure is borne by pore pressure at the deeper point; this point is the overpressure point [8-11]. The formula is:

$$(P_0)_A - (P_p)_A = (P_0)_B - (P_p)_B \quad (4)$$

In the formula, P_0 is overburden pressure, P_p is the pore fluid pressure.

In the normal circumstances, the porosity of mudstone will increase as exponential function with depth, that is:

$$\phi_{shA} = \phi_{sh0} \times e^{-CH_A} \quad (5)$$

In the formula, ϕ_{sh0} and ϕ_{shA} are respectively the porosity of mudstone of the surface and the arbitrary depth. C is the coefficient of compaction, H_A is the altitude location of A. Because of the linearly relationship between the porosity of mudstone and the interval transit time, the porosity in formula (5) can be replaced by the data of interval transit time. And the following formula can be obtained by taking the natural logarithm on both sides of formula (5):

$$\ln \Delta t_{shA} = \ln \Delta t_{sh0} - CH_A \quad (6)$$

Or:

$$H_A = -\frac{1}{C} \ln \frac{\Delta t_{shA}}{\Delta t_{sh0}} \quad (7)$$

After fitting with the acoustic logging data that measured in actual mudstone formation, the Δt_{sh0} , C and the normal compaction trend equation can be obtained [12-14].

After choosing the good normal compaction section and obtaining the normal compaction curve, we can come back to the formula (4). Assuming that the point A is in the normal compaction zone and point B in the overpressure zone, then the pore pressure of point A equals to the hydrostatic pressure. Further, if we consider the density of the overlying strata of both points is equal, the hydrostatic pressure and the overburden pressure are:

$$P_w = 10^{-3} \rho_w g H \quad (8)$$

$$P_0 = 10^{-3} \rho_b g H \quad (9)$$

In the formula, ρ_w is pore fluid density, g/cm³, ρ_b is the overlying formation density, g/cm³, H is depth, m.

Feeding formula (8) and (9) into formula (4) to obtain the general formula:

$$(P_p)_B = 10^{-3} \rho_w g H_B + 10^{-3} g (\rho_b - \rho_w) (H_B - H_A) \quad (10)$$

And feeding formula (7) into formula (10) to obtain the general formula:

$$P_p = 10^{-3} \rho_w g H + 10^{-3} g (\rho_b - \rho_w) \left(H - \frac{1}{C} \ln \frac{\Delta t_{sh}}{\Delta t_{sh0}} \right) \quad (11)$$

The formula (11) is for the pore pressure. Therefore, after knowing the coefficient of compaction C and the fitted value of surface interval transit time Δt_{sh0} , the formation pore pressure can be calculated from this equation.

3. Analysis of Application in Fuling area

Based on the theory and method described above, this paper conducted the logging evaluation of the pore pressure for a number of parameter well of Fuling area, also processed and valued the data of interval transit time of Well A according to the above method to establish a normal compaction trend. In the process of valuing, the main principles are: 1) Select the pure mudstone section on the basis of

natural gamma ray logging, spontaneous potential logging data and geological well log data, and remove the limestone of the Huanglong formation to reserve the thin mudstone layer which is considered to be the normal compaction section. 2) Take the stable layer section of the caliper log and remove the part that has obvious diameter shrinkage or extension to avoid the influence of drilling fluid on the acoustic transit time data. 3) Pick the average value of the interval transit time curve of mudstone strata rather than the peak value and the frequency hopping value when you are reading the value. And pay attention to the trend of the values of the acoustic logging curve of mudstone in case of reading some isolated high or low values. For the mudstone section that has high thickness and in the principle of taking less and essence, do pick the representative data points and avoid too much data gathering at the same depth. According to this principle, the normal compaction trend equation of Well A can be established (see fig 1):

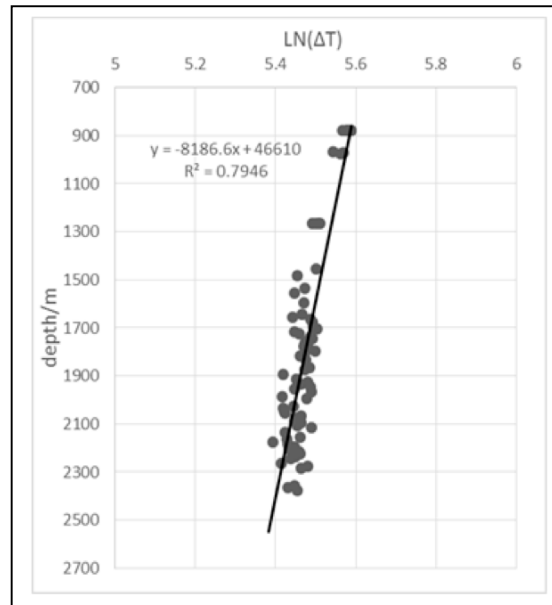


Figure 1. “the normal compaction trend” line of well A

The general equation between acoustic transit time Δt and depth H can be obtained by fitting this curve.

$$H = -8186.6 \times \ln(\Delta t) + 46610 \quad (12)$$

$$\ln(\Delta t) = 5.693 - 0.000021 \times H \quad (13)$$

At the same time, the theoretical value of interval transit time Δt_0 of mudstone strata in the surface environment can also be obtained. By feeding formula (13) with Δt_0 into formula (11), the continuous pore pressure data of Well A can be achieved (as shown in Figure 2).

Figure 2 shows the comparison between formation pore pressure and hydrostatic pressure that calculated by the equivalent depth method and the target layer from Longmaxi formation to Wufeng formation locates among 2326m-2415m. The overall overpressure characteristics of these target layers can be seen by calculating, and the upper 2200m and 2230m shows slightly overpressure too. But this part should be the result of the abnormal acoustic transit time that caused by the wellbore instability. The variation of lithology at 2300m can be seen from the natural gamma curve, and it makes the calculation of pressure abnormal that the interval transit time becoming smaller. The pressure ranges from 27Mpa to 35Mpa can be obtained after reading the pore pressure of target layer precisely. Therefore, to make ratio of pore pressure-to-hydrostatic pressure of the same depth can acquire the pressure coefficient 1.18-1.33. However, the error about 6% exists between the result and the pressure coefficient, which is 1.10-1.27, measured at Longmaxi formation to Wufeng formation of this well. But

the size of this error is allowed within the scope of works scope. So in this way, it is suitable to use “equivalent depth method” to calculate the formation pressure of Well A.

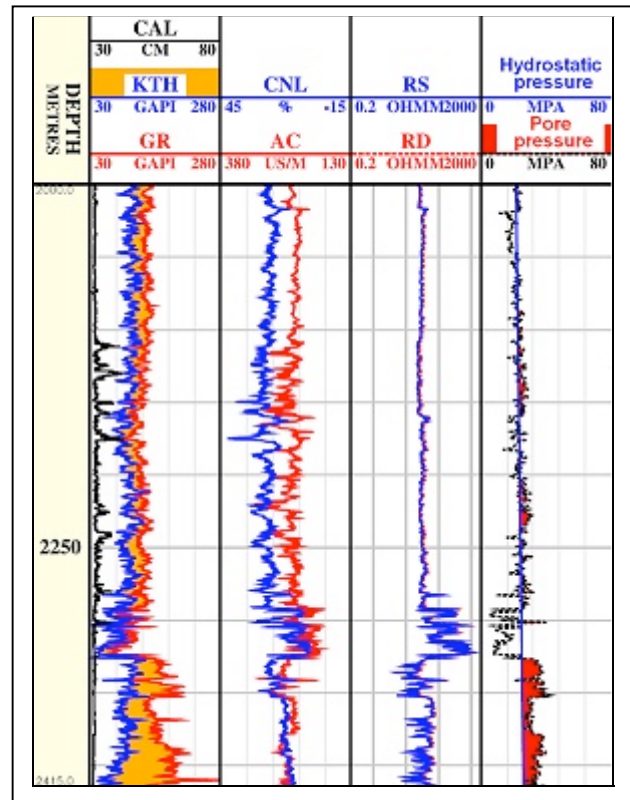


Figure 2. Calculation results of pore pressure in A well

The method can be used on the other exploratory wells, Figure 3 shows that all the error is less than 8%, the average error can be as small as 6.4% by combining the calculated result from Well A. The results indicate that "equivalent depth method" in calculating the pore pressure of Longmaxi formation in Fuling area has good results.

Figure 3. Comparison chart of calculated and measured formation pressure coefficient in Fuling area

Well	Depth	Pressure Coefficient		Error
		Calculated values	Measured values	
B	2475-2575	1.15-1.37	1.26-1.47	7.85%
C	2317-2418	1.2-1.47	1.28-1.50	4.48%
D	2512-2596	1.22-1.57	1.34-1.52	6.12%

4. Results and Conclusion

This paper contrasts the calculation method for well logging of pore pressure of shale gas reservoir, including “comprehensive interpretation method”, “Eaton method” and “equivalent depth method”. According to the characteristics of the study area data and on the basis of acoustic logging data with other related logging material, we selected the mudstone section that deposited stably and picked the “equivalent depth method” to establish a normal compaction trend line equation to obtain the pore pressure data of a single well. This method has a smaller amount of calculation and the solving efficiency is very high.

The results that calculated on shale gas reservoir of Longmaxi formation of Fuling area shows: The pore pressure calculation method proposed by this paper achieved good results in four wells and the calculation precision is relatively high. Therefore, it is applicable to the evaluation and interpretation of

logging data of shale gas reservoir in Fuling area.

ACKNOWLEDGEMENT

Declared none.

Conflict of interest

Declared none.

Reference

- [1] Fan Honghai. A new integrated pore pressure evaluation method for shale-sand formations [J]. PETROLEUM EXPLORATION AND DEVELOPMENT, 2002, 29(1): 90-92.
- [2] D.H. Eberhart, M.D. Zoback. Empirical relationships among seismic velocity, effective pressure, porosity, and clay content in sandstone [J]. Geophysics, 1989, 54(1): 82
- [3] J.L. Allxant. Explicit pore-pressure evaluation: concept and application [J]. SPE Drilling Engineering, 1991, September.
- [4] G.Y. feng, J.X. jian. Accurate prediction of formation pore pressure and its application [J]. CHINA OFFSHORE OIL AND GAS, 2004, 16(1): 36422.
- [5] C.Q. Zhong. Research Review on the abnormal pressure formation mechanism [J]. Natural Gas Exploration and Development, 2001, 24(4): 38-46.
- [6] D. Ciqian. Mine geophysical [M]. CHINA UNIVERSITY OF PETROLEUM PRESS, 2002: 93-95.
- [7] B.A. Eaton. Graphical Method Predicts Geopressure worldwide [J]. World Oil, June, 1972: 51-56.
- [8] F. Honghai. Determination and Regression of Overburden Pressure Gradient [J]. PETROLEUM DRILLING TECHNIQUES, 2002, 30(6): 6-8.
- [9] Z. Chuanjin. Prediction of Formation Pore Pressure in Wild Cat Wells [J]. Petroleum Drilling Techniques, 2002, 30(3): 1314.
- [10] W. Maoan, C. Chao. New approach for pore pressure prediction [J]. Oil & Gas Geology, 2007, 28(3): 395-400.
- [11] Y Rong. Quantitative evaluation of abnormal formation pressure [J]. FAULT — BLOCK OIL & GAS FIELD, 2001, 8(3): 25-28.
- [12] L. Shansheng. Log Evaluation about Formation Pore Pressure of Boxing Subsag [J]. WELL LOGGING TECHNOLOGY, 2013, 37(2): 169-172.
- [13] Z. Xing, H. Shiming. Prediction method of shale formation pore pressure [J]. Fault-Block Oil & Gas Field, 2007, 14(1): 24-26.
- [14] S. Bo. A new method of formation pore pressure prediction in Northeast Sichuan area [J]. Journal of Oil and Gas Technology, 2011, 33(8) f: 96-98, 103.